

Voltage Source Converter (VSC) IEEE PES Winnipeg Tutorial

December 18, 2012

Randy Wachal Manitoba HVDC Research Centre rww@hvdc.ca

MANITOBA HYDRO INTERNATIONAL MANITOBA HVDC RESEARCH CENTRE MANITOBA HYDRO TELECOM W.I.R.E. SERVICES

Acknowledgements:

NSERC Power System Simulation Chair program at University of Manitoba ..

MHRC Staff Dr. Farid Mosallat and Juan Carlos Garcia

Cigre DC Grid Working Groups B4-55, 56 57 58 59 and 60 ..

ABB Siemens and Alstom Grid

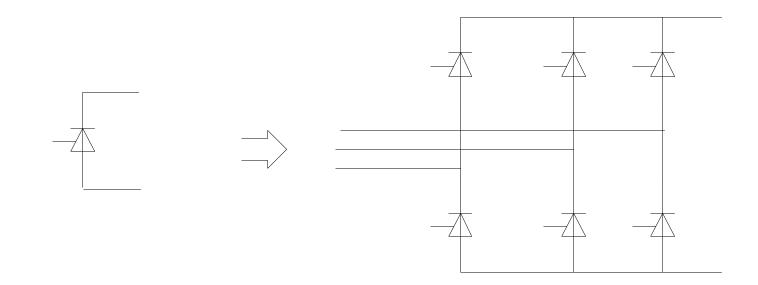
MANITOBA HYDRO INTERNATIONAL MANITOBA HVDC RESEARCH CENTRE MANITOBA HYDRO TELECOM W.I.R.E. SERVICES

VSC Tutorial

VSC Converter Theory Basics VSC Control and Modelling VSC system simulations Start –up; DC Fault DC Grid Test Case Cigre B4-57/58

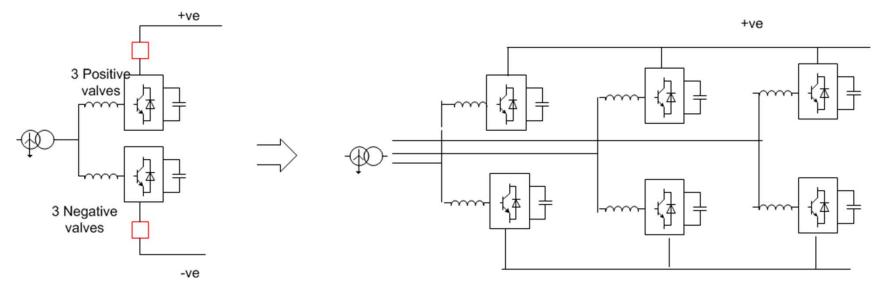
MANITOBA HYDRO INTERNATIONAL MANITOBA HVDC RESEARCH CENTRE MANITOBA HYDRO TELECOM

Introductory Basics: LCC Single line





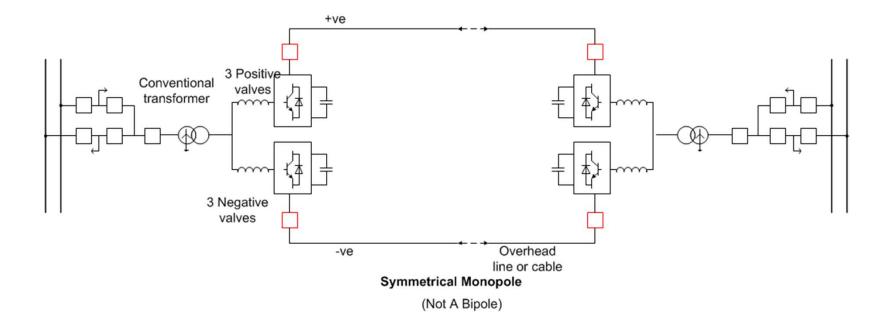
VSC: Single Line Diagram Format



-ve

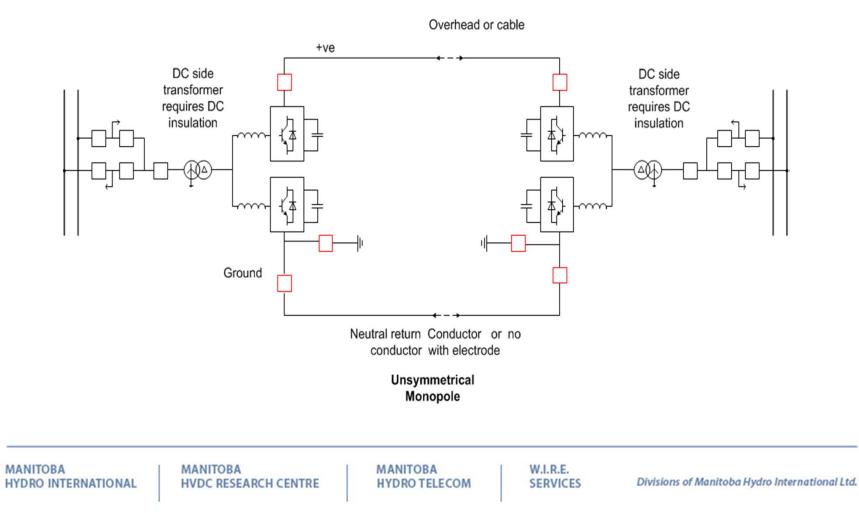


Symmetrical HVDC Monopole

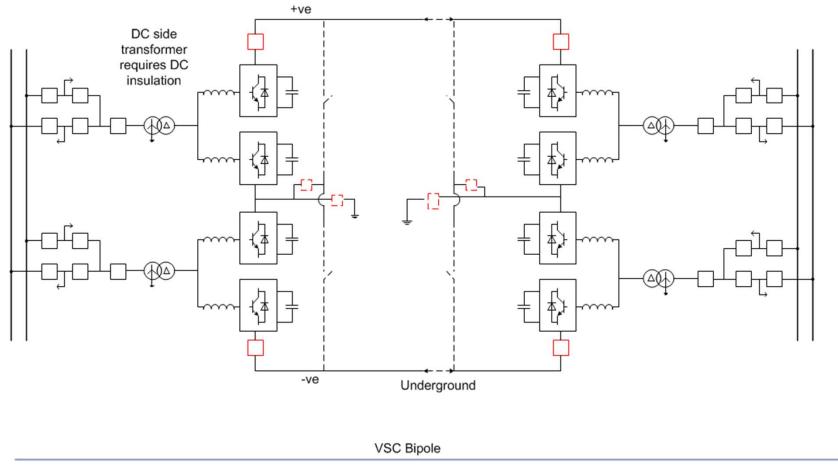




VSC: Unsymmetrical Monopole



VSC: Bipole Configuration



MANITOBA MANITOBA MANI HYDRO INTERNATIONAL HVDC RESEARCH CENTRE HYDR

MANITOBA HYDRO TELECOM W.I.R.E. SERVICES

LCC - VSC Comparison

LCC HVDC

Mature Technology "Requires" strong ac system Lower losses 0.8% per converter Requires 60% reactive power AC-DC system interactions Harmonics Commutations failure **Special Transformers** Multi terminal operation possible but hard Controlled DC Current to zero (Idref=0) Dc voltage + to - as alpha changes rectifier to inverter

VSC HVDC

Rapid growth Helps ac system Control real and reactive power independently Losses reducing 1.1-1.2% per converter No Commutation failure Less Special Transformers Flexible Dispatch Harmonics with MMC no issue DC Grid (multi-terminal) possible DC voltage is a constant polarity DC Line faults are problematic

MANITOBA HYDRO INTERNATIONAL

Multi Terminal

For LCC:

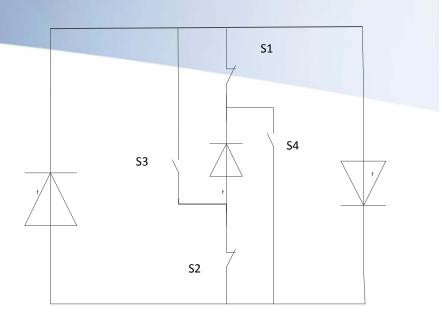
Rect α < 90 Vdc +ve

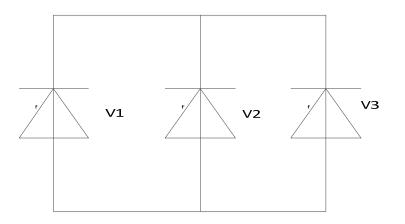
INV $\alpha > 90$ Vdc -ve

To change Conv 2 from Rect to Inv you must flip the thyristor

For VSC:

Power Flow is controlled by control signals only







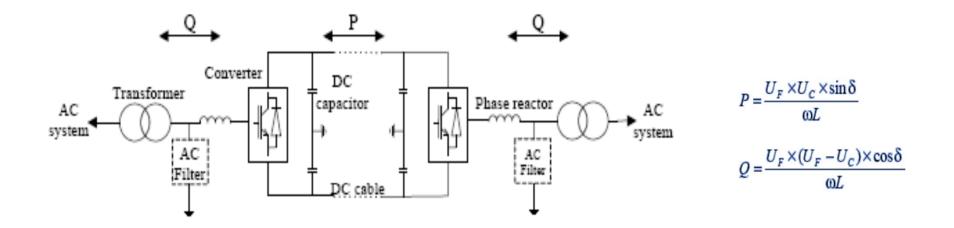
VSC Technology is very flexible

VSC technology can control two variables together real power and reactive power VSC can generate an AC Waveform.... Black start or island mode possible Many dispatch options available • Real Power set point in or out + or -

- Real Power set point in c
 Use power to control DC voltage Vdc
- In island mode : use power to control frequency
- Reactive Power Q set point in or out + or -
- Use Q to control Vac magnitude Grid or islanded Mode...
- Other control targets are possible..

MANITOBA	MANITOBA	MANITOBA	W.I.R.E.	Divisions of Manitoba Hydro International Ltd.
HYDRO INTERNATIONAL	HVDC RESEARCH CENTRE	HYDRO TELECOM	SERVICES	

VSC Operation

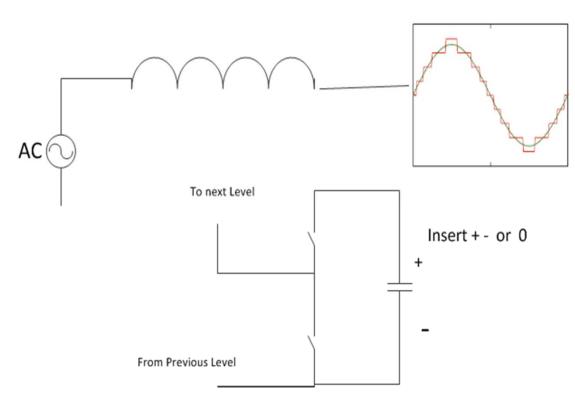


We tend to think of LCC from AC side to rectifier and generate Dc voltage

For VSC ; think from the DC side.. Assume DC Capacitors are charged The capacitor voltages are used to piecewise build ac voltage We the ac voltage waveform and the ac system voltage now we can transfer energy to charge Dc capacitor(s)



Transfer P & Q across Reactor



Use DC capacitor voltage (Ud) to build an ac Voltage waveform Uc

Exchange P based on δ • $\uparrow \delta$ P into Converter Ud \uparrow • $\downarrow \delta$ P from Converter Ud \downarrow

Exchange Q based on |Uc|
↑ |Uc| Q flows into system
↓ |Uc| Q flows from system

MANITOBA
HYDRO INTERNATIONALMANITOBA
HVDC RESEARCH CENTREMANITOBA
HYDRO TELECOMW.I.R.E.
SERVICESDivisions of Manitoba Hydro International Ltd.

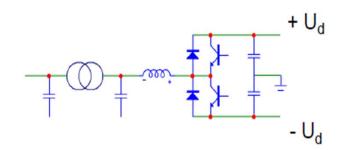
History of VSC Development: ABB, Siemens and Alstom Grid

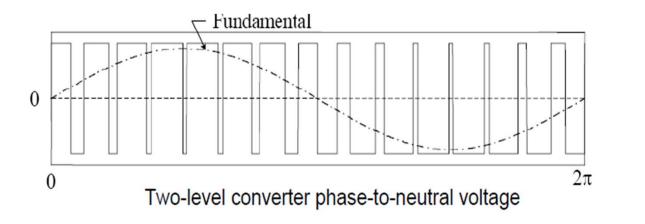
- VSC Rapid Growth and continue to change
- Many projects but few projects have the same design
- An MMC type configuration appears to be the "winner" but many marketplace has variations
 - Not unlike LCC technology 25 years ago
- The Final VSC configuration is not decided
 - and may never occur.

HVDC Light Historical review, 1997-2001

Two-level Converter, Generation 1

- Converter losses 3 %
- High switching frequency
- Filters required



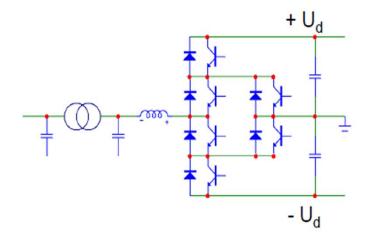


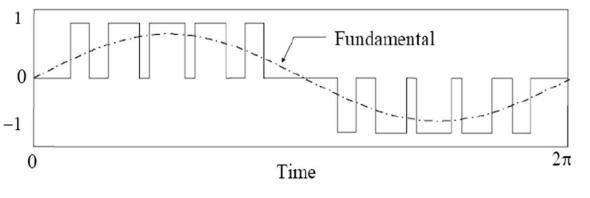
ernational Ltd.

HVDC Light Historical review, 2002-2004

Three-level Converter, Generation 2

- Converter losses 1.7 %
- Switching frequency reduced
- Harmonic generation improved





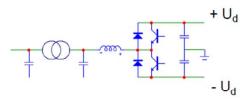
Three-level converter phase-to-neutral voltage

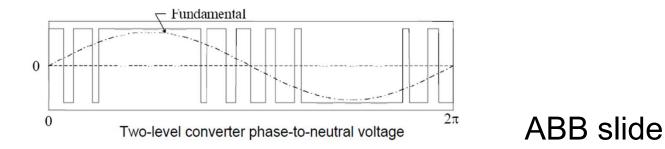
ational Ltd.

PWM Based VSC

HVDC Light Historical review, 2005-2009

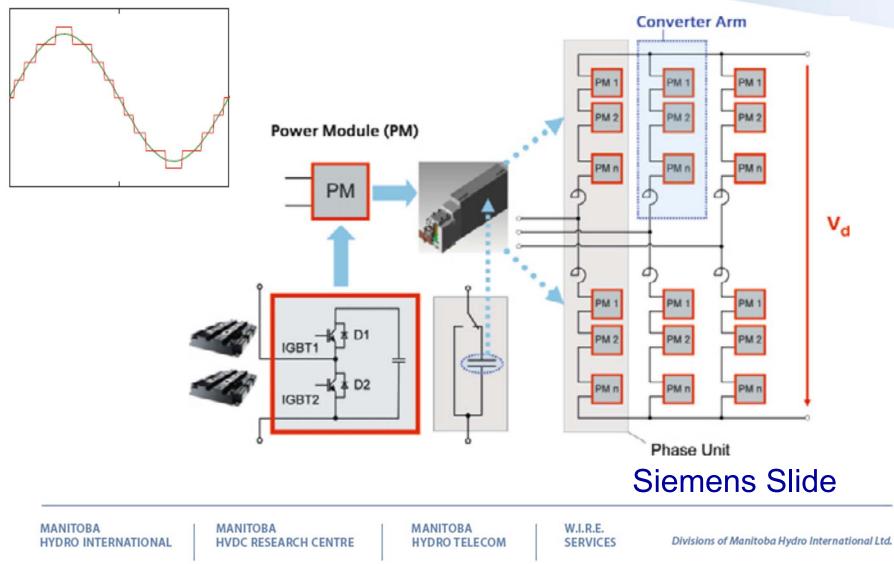
- Two-level Converter, Generation 3
- Converter losses 1.7 % By optimized IGBT and drive
- Lower switching frequency
- Harmonic generation maintained



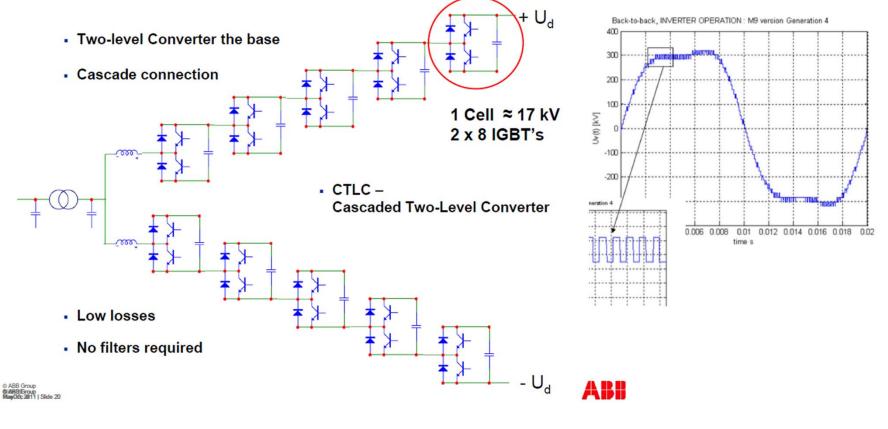




¹/₂ Bridge Multi Module Converter MMC



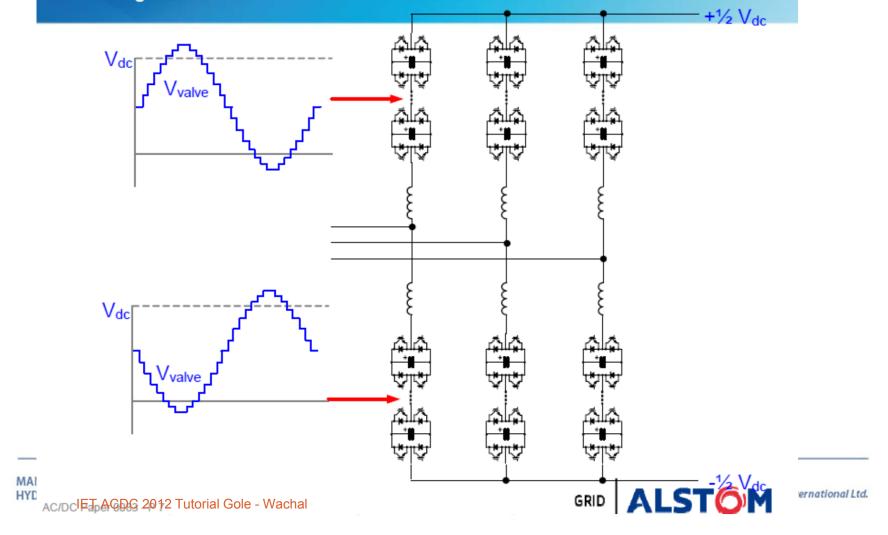
HVDC Light Generation 4



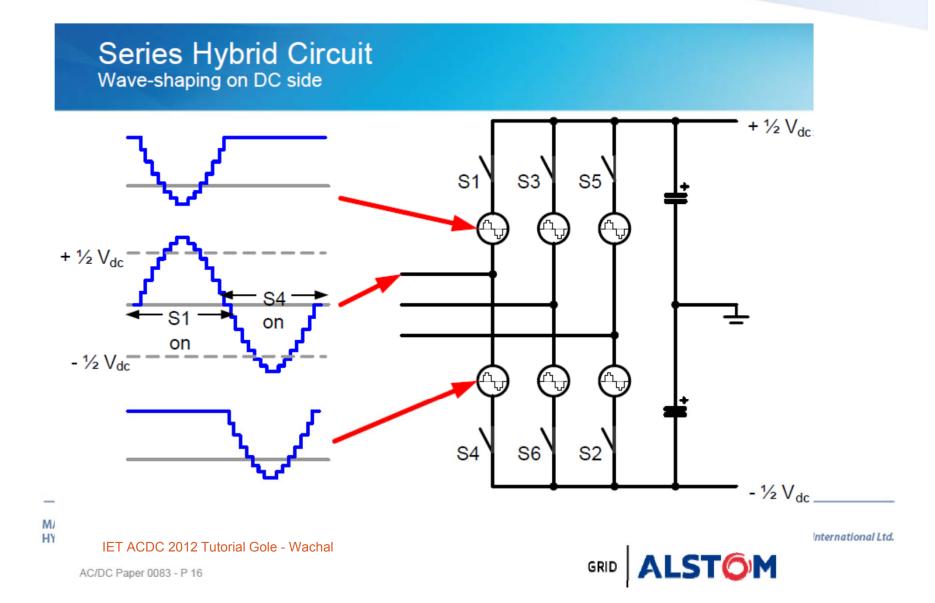


Full Bridge MMC

Modular Multi-Level Converter (MMC) Full-bridge version



One possible Hybrid Configuration



VSC Control and Modelling

- Control system organization
- Look at impact of diode in configuration
- High Level Control
 - D Q controller development

Development of Voltage reference signals based on dispatched orders

Lower level control

Valve fire pulses (IGBT firing pulses)

Capacitor energy balancing

 MANITOBA
 MANITOBA
 MANITOBA
 W.I.R.E.

 HYDRO INTERNATIONAL
 HVDC RESEARCH CENTRE
 HYDRO TELECOM
 SERVICES
 Divisions of Manitoba Hydro International Ltd.

Models For VSC MMC system

EMT and RMS transient (Dynamic and loadflow) type models are required

Lots of VSC configurations to consider

- PWM based (all series devices in Valve switch together)
- ¹/₂ bridge MMC
- 1/2 bridge MMC with PWM (cascaded two level converter CTLC)
- Full bridge MMC
- Hybrid mixtures of series values, $\frac{1}{2}$ and full bridges

Traditional 'emt' solution methods not effective

Emt simulation speed is dependent on number of electrical nodes (size of simulation matrix)

MMC configurations increase electrical nodes exponentially

- LCC and PWM VSC
 - 6 nodes per 3 phase valve
 - entire valve arm (xx series devices) switch together
- MMC

MANITOBA

HYDRO INTERNATIONAL

• Valve may have 400 levels (each switching independent)

MANITOBA

HYDRO TELECOM

W.I.R.E.

SERVICES

Divisions of Manitoba Hydro International Ltd.

• 400*6 = 2400 nodes for 1 converter

Compare 6 to 2400 simulation issue is evident ...

HVDC RESEARCH CENTRE

MANITOBA

VSC System Control Model & Levels

• Dispatch What is the target of Converter ?

- Power Set or Dc voltage (grid mode)
- Ac voltage reference or MVar set (grid mode)
- Frequency reference (P) and Ac Voltage (Q) (island mode)
- Other P& Q strategy

• High Level Controls

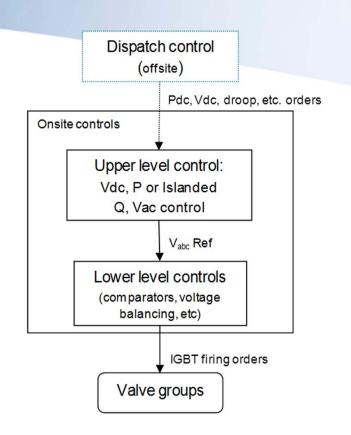
- Based on dispatch set points (Inputs)
- Droop setting to allow autonomous control
- d-q control will generate Vref a, b and c (outputs)
- Voltage and current limits applied

Lower Level Controls

- Inputs Vref signals
- Valve specific configurations

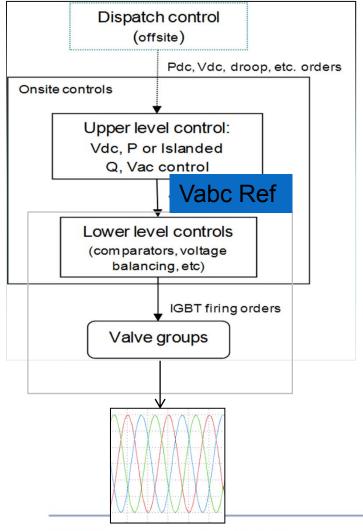
($\frac{1}{2}$ bridge MMC, $\frac{1}{2}$ bridge MMC with PWM, full bridge, etc.)

- Capacitor balancing algorithm(s)
- Circulating current suppression algorithm(s)
- Generates gate pulses and the ac waveforms





Control Hierarchy



Natural separation occurs Higher Lower level Controls

Regardless of Dispatch Orders Higher Level controls develop

Vref A Vref B and Vref C outputs

Regardless of converter valve implementation Lower Level controls use the VREF inputs to generate the gate pulses to produce

Va Vb and Vc

Lower level controls are unique for valve topology and will have ancillary control

- Capacitor balance
- Circulating current suppression

MANITOBA HYDRO INTERNATIONAL MANITOBA HVDC RESEARCH CENTRE MANITOBA HYDRO TELECOM

Impact for VSC System Models

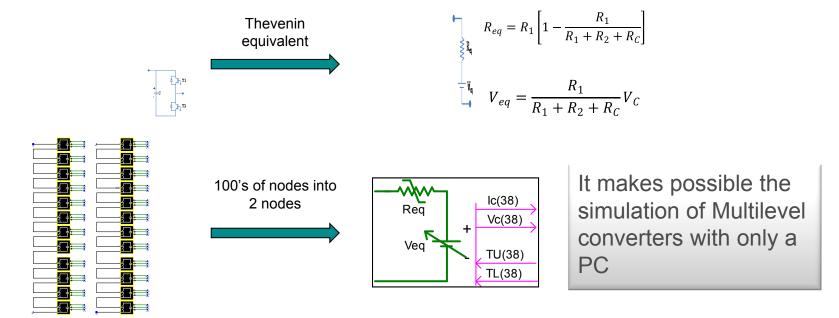
- Dispatch and Higher Levels Controls remain same regardless of Converter implementation
 - Generic or public domain models
 - Vendor specific (IP) models
- Lower Level Controls unique for different types of converter
 - Different Power electronics and control algorithm
 - Different Capacitor balance algorithm
 - Different Circulation Current suppression algorithm
 - Generic or public domain models
 - Vendor specific (IP) models
 - Different level of details for each lower level models
 - Full emt, detailed equivalent, firing pulse RMS

From a Simulation Study Point View

Choose the appropriate Lower Level Model for your study ... How ???

New Model Techniques required

Computationally efficient model developed by Simulation Chair University of Manitoba



U. N. Gnanarathna, A. M. Gole, and R. P.Jayasinghe, "Efficient Modeling of Modular Multilevel HVDC Converters (MMC) on Electromagnetic Transient Simulation Programs," IEEE Transactions on Power Delivery, vol.26, no.1, pp.316-324, Jan. 2011

MANITOBA MANITOBA MANITOBA MANITOBA MANITOBA W.I.R.E. HYDRO INTERNATIONAL HVDC RESEARCH CENTRE HYDRO TELECOM SERVICES Divisions of Manitoba Hydro International Ltd.

Start up Concerns

Initial Energization

Transformer

MANITOBA

HYDRO INTERNATIONAL

• MMC Capacitors (Precharge capacitors to 1.41*ELL via diodes)

MANITOBA

HYDRO TELECOM

W.I.R.E.

SERVICES

Divisions of Manitoba Hydro International Ltd.

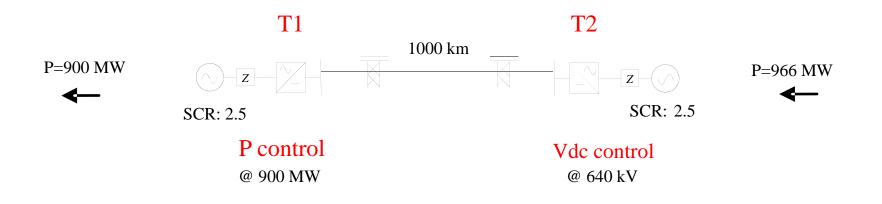
DC Line or DC Cable

MANITOBA

HVDC RESEARCH CENTRE

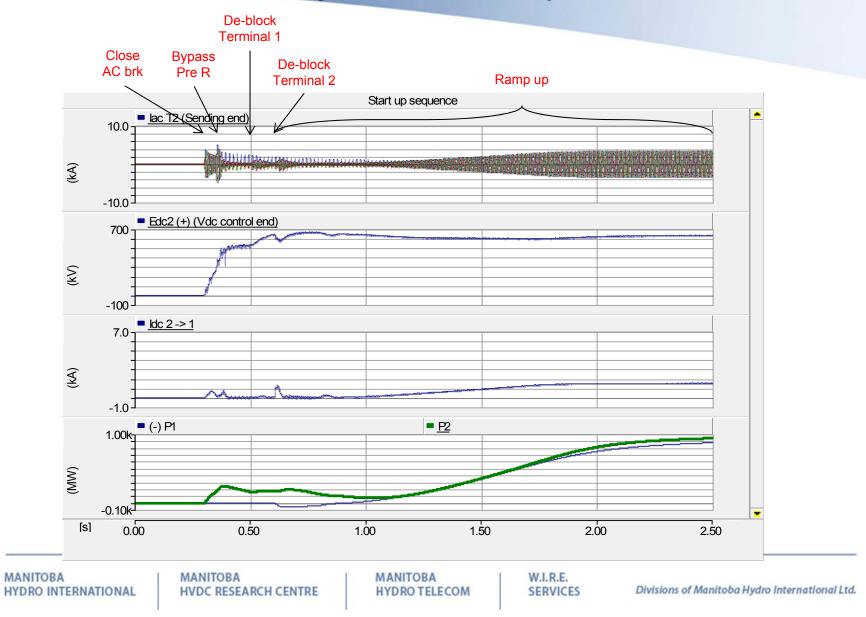
Use start-up resistor to limit current. Short resistor with by pass switch Deblock pulses Conv 1 and then Conv 2 Ramp power to desired setpoints

Session 3: VSC system start up





Session 3: VSC system start up

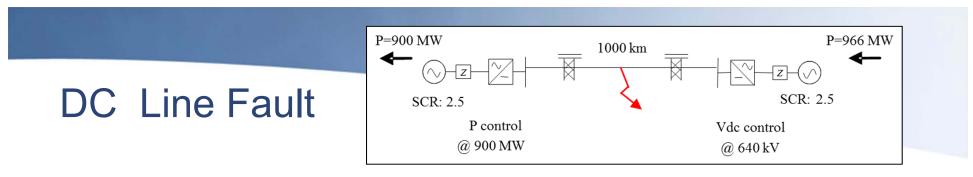


Summary Issues VSC Start-up

- During start-up energization of both transformers and all capacitors therefore Larger Inrush
- Inrush resistor commonly added with bypass switch
- Diodes: with no firing pulse and diodes will conduct resulting in a Dc voltage
- VDC=1.41 peak of Vac L-L
 - (charge capacitors and line (or Cable)



rww1



VSC scheme with overhead line (based on Caprivi)

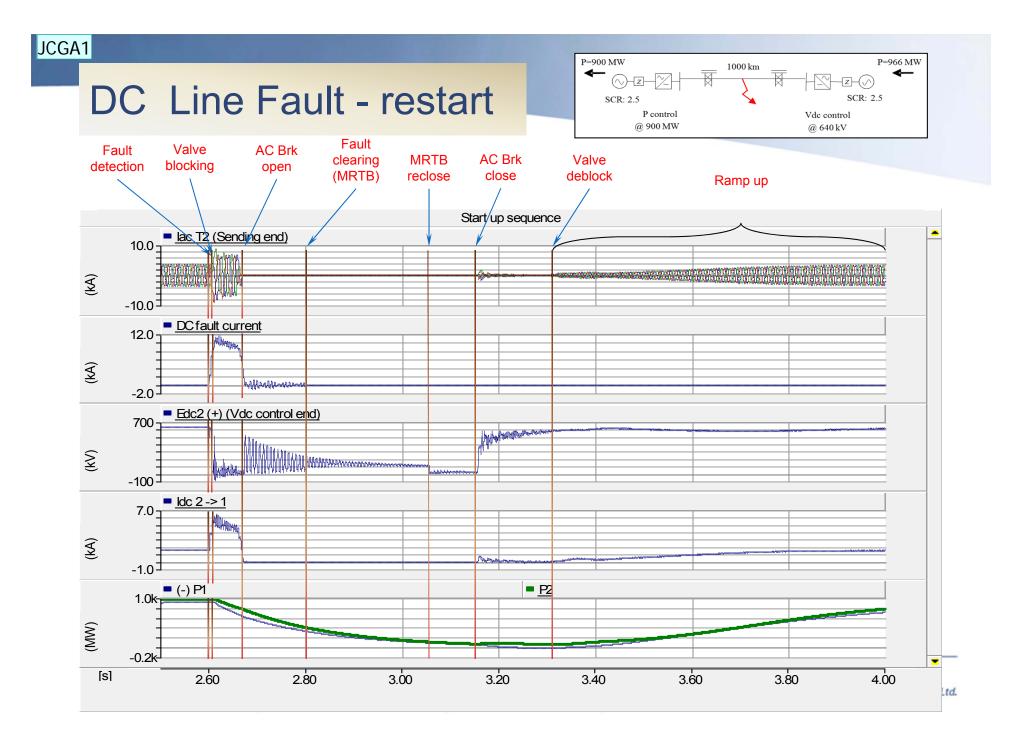
no Dc Fast (4 msec) breaker installed

Resonant DC Breaker (50-75 msec installed)

- On DC fault.. Block firing pulse.. MMC capacitors cannot discharge into line but diodes will continue to commutate and feed DC fault (as 6P LCC rectifier)
- Open AC breaker .. Remove 6p rectifier diode current
- DC line will discharge slowly.. Based on the R/L circuit of the Dc line will keep the post fault DC current present for seconds up to a couple of minutes .

A dc switching action is required to allow Dc fault recovery

MANITOBA HYDRO INTERNATIONAL MANITOBA HVDC RESEARCH CENTRE MANITOBA HYDRO TELECOM W.I.R.E. SERVICES

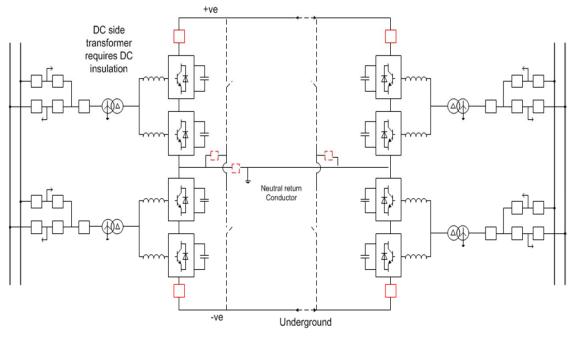


Summary for VSC Dc Line Faults

- Pulse Blocking removes discharge of capacitors quickly
- AC breaker is required to open to remove 6P diode current.
- For a weak ac system .. DC fault draws fault current from AC bus. dc fault = ac fault
- Post fault residual dc current requires resonant Dc breaker
- For recovery inrush.. MMC capacitors are already charged
- Power ramp rate is determined by ac system strength not dc controls.

Neutral Return

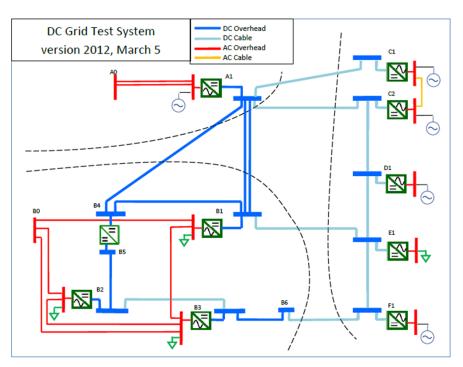
- Eliminate ground currents
- Increased line losses
- DC voltage offset at remote station.. Requires more dc insulation
- Neutral current can be controlled to zero by bipole controller
- During pole outage, the pole conductor can be used to reduce losses.



VSC Bipole



DC Grid Modelling Test System (B4-58)



et a service a service de la service

B4-57 has developed T-line and cable parameters for test case

A base PSCAD and EMPT-RV test cases are available.

Models are changing ...

Test Case alternatives

- Monopole
- Bipole with neutral return
- Bipole with ground/ sea electrodes.

MANITOBA HYDRO INTERNATIONAL MANITOBA HVDC RESEARCH CENTRE MANITOBA HYDRO TELECOM

Thank you...

Questions?

