# VFD Installations and Applications 

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## Agenda

## Part 1:

- Harmonic Mitigation
- Methods to reduce Ithd, Vthd
- Line reactors and DC link chokes
- Active Rectifier Applications
- Downhill conveyors
- Centrifuges
- Fans
- Dynamometers
- Fibers
- Paper mills
- Cranes
- Active Rectifier Operation
- What about Power Factor?


## Part 2:

- Motor speed vs max load / cooling, use of motor RTDs
- Overspeed with fans / pumps and increase in torque and power
- Min speed with pumps
- SCCR for drives
- HRG vs solid ground
- Shaft grounding brushes / bearing currents
- Load reactors on the output
- Wiring on input / output
- Insulation types
- Conduit, tray
- Type (VFD, individual wires)
- Control wiring management

Part 1

Harmonic Mitigation

## Harmonics - What can be done?

Solutions typically used

## LV Drives

- Line Reactors or isolation transformers
- DC Link Chokes
- Passive Harmonic Filters
- Active Harmonic Filters
- Multi-Pulse (parallel bridges)
- 12P, 18P
- AFE (ULH)


## MV Drives

- Multi-Pulse (series or series/parallel bridges)
- 12P, 18P, 24P, 36P, 72P
- AFE (ULH)


## General Block Diagram of an AC Drive



## General Block Diagram of an Industrial AC Drive



## 6-Pulse Drive, no mitigation

80-120\% Ithd


Basic Converter


## 6-Pulse Drive with Line Reactor and/or Link Choke



## 6-Pulse Drive with Passive Harmonic Filter

## 5-10\% Ithd



Passive Harmonic Filter

(supplies harmonics)


## How is Multi-Pulse accomplished?

| Input Current <br> Pulses / Cycle | Number of 6- <br> Pulse Bridges <br> (secondaries) | Number of <br> Phases <br> (wires) | Phase Shift <br> Between <br> Bridges | Harmonic <br> Pairs |
| :---: | :---: | :---: | :---: | :---: |
| 6 | 1 | 3 | -- | $6 \mathrm{k} \pm 1$ |
| 12 | 2 | 6 | 30 | $12 \mathrm{k} \pm 1$ |
| 18 | 3 | 9 | 20 | $18 \mathrm{k} \pm 1$ |
| 24 | 4 | 12 | 15 | $24 \mathrm{k} \pm 1$ |
| 36 | 6 | 18 | 10 | $36 \mathrm{k} \pm 1$ |
| 48 | 8 | 24 | 7.5 | $48 \mathrm{k} \pm 1$ |
| 72 | 12 | 36 | 5 | $72 \mathrm{k} \pm 1$ |
| = multiple of 6 | $=$ Pulses /6 | $=$ Pulses /2 | $=360 /$ Pulses | $\mathrm{k}=1,2,3, \ldots$ |

## 12-Pulse Drive: Series or Parallel Bridges



Parallel Bridges

*Series Bridges
(cancels harmonics)


## 12-Pulse Drive: Pseudo 12-Pulse

$10-15 \%$ Ithd $\quad$ Split the drive load into two, somewhat equal parts.


Or use two zig-zag transformers: One zigs $+15^{\circ}$, the other zags $-15^{\circ}$ One spare can be used either way.


Or use one Dy transformer and a line reactor. Match the impedances.

## 18-Pulse Drive: Series or Parallel Bridges



Parallel Bridges


* used for MV drives
*Series Bridges


## 24-Pulse Drive: Series / Parallel Bridges


*Series / Parallel Bridges, 24P
(cancels harmonics)


* used for MV drives


## 36-Pulse Drive: Series / Parallel Bridges

3-4\% Ithd

*Series / Parallel Bridges, 36P
(cancels harmonics)


* used for MV drives


## How does it help?



## 6-Pulse with Active Harmonic Filter



Active Harmonic Filter


## 3-Phase Drive with Active Front End




* used for MV drives


## Line Reactors and DC Link Chokes

Line Reactors on the Input to a Drive


## Let's look at some voltages and current.



## Rectifier w/o DC Link Choke



## Rectifier w/o DC Link Choke



## Rectifier w/o DC Link Choke



## First Current Pulse



## Second Current Pulse



## Addition of DC Link Choke



## -or- an Addition of AC Line Reactor



## Rectifier with DC Link Choke



## Rectifier with DC Link Choke



## 6-Pulse Drive, no mitigation

80-120\% Ithd


Basic Converter


## 6-Pulse Drive with Line Reactor and/or Link Choke

$30-40 \%$ Ithd


AC Line Reactor


Link Choke and Reactor

## How else does a line reactor help?

Recovery from a sag or interruption


Less likely to blow a fuse or trip a CB.


## How else does a line reactor help?

PFCC energization


Less likely to blow a fuse or trip a CB or trip on OV.


## Low Impedance Source (a very big transformer)



No LR or LC


Less stress on diode bridge - longer life.
Less bus ripple - longer cap life.
Less likely to trip on excessive bus ripple.

Rule of thumb: if $x f m r$ is $>20 x$ kVA rating of drive, add a line reactor!


## Open Delta Source - Unbalanced Impedances



No LR or LC

Less stress on diode bridge - longer life. Less bus ripple - longer cap life. Less likely to trip on excessive bus ripple.




## Unbalanced Line Voltages



No LR or LC


Less stress on diode bridge - longer life. Less bus ripple - longer cap life.
Less likely to trip on excessive bus ripple.


## Problem with too much Line Reactor \% ( $\max =5 \%)$

Low DC bus voltage means:
Low motor voltage (at max speed) Higher motor current
More heating Shorter life
\% Vbus vs Load (lsc/lload = 47)


## How does motor load affect I(THD)?



## NOTES:

I(THD) = Iharm / Ifund
I(THD) increases as load decreases

Ifund decreases as load decreases Iharm decreases as load decreases
(drive is at full speed)

## Vthd vs Load - Zoomed In



100hp drive on 250kVA xfmr, 6\%

Active Rectifier Applications

## Quadrants of Operation

Braking in reverse
direction: stopping,
plugging, lowering hoist,
generator action

## Special applications that require regeneration

- Downhill conveyors
- Centrifuges
- Cooling and ID fans
- Dynamometers
- Fabrics - Kevlar
- Paper mills
- Cranes
- Reasons:
- Continually braking (reverse torque)
- Braking or slowing down high inertia loads
- Emergency stopping for safety
- Dynamic braking dissipates the energy as heat in a resistor
- Regenerative braking sends the energy back into the power lines for other loads to use
- Constant braking torque throughout the speed range


## Shipyard Cranes



## Cooling Fans



## Downhill Conveyor




## Pump Jack

## CONSUMIIING



## Paper Mill



## Fibers such as Kevlar



Active Rectifier Operation

## 3-Phase Drive with Active Front End




* used for LV and MV drives


## Active Rectifier (AFE, ULH) AC Drive

## Active Rectifier

Synchronous Rectifier Synchronous Converter Active Front End, AFE Regenerative Unit, RGU
Ultra-Low Harmonic, ULH
IGBT Supply Unit, ISU


## Just Like Two DC Voltage Sources



Relative voltage magnitudes and resistance determine current magnitude and direction of power flow

## Two AC Voltage Sources

Direction of power flow


Relative voltage magnitudes and phase angles determine current magnitude, PF, and direction of power flow

## Current and Power Flow with an Inductor



$$
\overline{\mathrm{Ix}}=\frac{\overline{\mathrm{Vx}}}{\overline{j X}}=\frac{V x}{2 \pi f \mathrm{~L}}<-90
$$



## $\Theta=0^{\circ}$, Vafe $=100 \mathrm{Vpk}$, Current lags by $90^{\circ}$


["

## Current and Power Flow with AFE

By adjusting $V_{a}$ and $\theta$, you can control $\mathrm{I}_{\mathrm{L}}$ and $\beta$.


Fixed
Voltage and Angle

> Adjustable Voltage and Angle

$$
\mathrm{L} \angle \beta^{\circ}=\frac{\left(\mathrm{V}_{\mathrm{L}} \angle 0^{\circ}-V_{\mathrm{a}} \angle \theta^{\circ}\right)}{\mathrm{X}_{\mathrm{L}} \angle 90^{\circ}}
$$

## $\theta=0^{\circ}$, Vafe $=100$, Vline $=100$



Zero Current Zero Watts

$$
\xrightarrow[\text { Vafe }]{\text { Vline }}
$$

## $\theta=0^{\circ}$, Vafe $=90$



Lagging Current Zero Watts

## $\theta=0^{\circ}, \operatorname{Vafe}=100$




## $\theta=0^{\circ}$, Vafe $=110$



Leading Current Zero Watts

## $\theta=0^{\circ}, \operatorname{Vafe}=100$




## $\theta=-17^{\circ}$, Vafe $=100$



Lagging Current $>0$ Watts

## $\theta=-17^{\circ}$, Vafe $=105$



Unity PF Current $>0$ Watts

## $\theta=-17^{\circ}$, Vafe $=110$




## $\theta=-17^{\circ}$, Vafe $=105$



Unity PF Current $>0$ Watts

## $\theta=0^{\circ}, \operatorname{Vafe}=100$




## $\theta=+17^{\circ}$, Vafe $=105$



Unity PF Current <0 Watts

## $\theta=0^{\circ}, \operatorname{Vafe}=100$




## Ratio of Vafe to Vline vs Degrees



## Vector Loci for Unity PF



Vafe $=$ Vline $/ \cos (\theta)$

## AFE Converter

## Motoring

- unity power factor
- I and V in-phase
- I(THD) = 3.6\%


## Regenerating

- unity power factor
- I and V 180 deg out-ofphase
- I(THD) = 3.6\%

Voltages shown are Line to Neutral

Iline Vline Vafe


## AFE Line Notches without LCL Filter





Voltages shown are Line to Line
$75.00 \mathrm{~m} \quad 80.00 \mathrm{~m} \quad 85.00 \mathrm{~m} \quad 90.00 \mathrm{~m} \quad 95.00 \mathrm{~m} \quad 100.00 \mathrm{~m}$

## Line Notching



IGBT is on, creating line-to-line short circuit
Current in line reactor is increasing, storing energy in the reactors
Load is discharging the DC bus cap

## Line Notching



IGBT is off
Current in line reactor is charging the DC bus cap
Reactor energy is transferred to DC bus cap

## Line Notching



Blue = DC bus cap voltage
Red $=$ Current in line reactor
Green $=$ IGBT on/off signal

## Customer's 120V supply for office area

Without LCL Filter, AFE stopped


## Without LCL Filter, AFE running



With LCL Filter,
AFE running


## AFE Line Notches Reduced with LCL Filter



## Control of Vdc bus



Note the following:
The average current in the DC Bus Caps, Icap = Iafe - Iinu
Normally Icap $=0$, so Iinu $=$ Iafe
If the load increases:
Vcap decreases, and control increases Iafe to bring Vcap back to normal
If the load decreases or reverses:
Vcap increases, and control decreases or reverses Iafe to maintain Vcap

## AFE Rectifier with LCL Filter

## Advantages:

- Very low line harmonics, 3-4\% Ithd
- Unity PF
- Can operate with leading PF
- Sags will not affect motor voltage
- Possible to compensate for voltage drop along long leads
- Full power regeneration continually
- Constant torque braking at all speeds
- Fast stopping
- All in a small package without extra hardware!


Active Converter removes low frequencies by not creating them $<1 \mathrm{kHz}$
LCL filter (passive filter) removes high frequencies $>1.2 \mathrm{kHz}$ (current and voltage)
Power factor adjustable from 0.85 (leading or lagging) to 1.0
Full output voltage is available with $80 \%$ input voltage $(400 \mathrm{VIn}=480 \mathrm{VOut})(3300 \mathrm{VIn}=4160 \mathrm{VOut})$
Full regenerative capability
No phase shifting transformer required
Less affected by line imbalance

## IEEE 519-2014, Annex C

## Table C-1—Recommended limits on commutation notches

|  | Special <br> applications | General <br> system | Dedicated <br> system |
| :---: | :---: | :---: | :---: |
| Notch depth | $10 \%$ | $20 \%$ | $50 \%$ |
| Notch area $\left(\mathrm{A}_{\mathrm{N}}\right)^{\mathrm{c}, \mathrm{d}}$ | 16400 | 22800 | 36500 |

${ }^{a}$ Special applications include hospitals and airports.
${ }^{\mathrm{b}}$ A dedicated system exclusively supplies a specific user or user load.
${ }^{\text {c }}$ In volt-microseconds at rated voltage and current.
${ }^{\mathrm{d}}$ The values for $A_{\mathrm{N}}$ have been developed for 480 V systems. It is necessary to multiply the values given by $\mathrm{V} / 480$ for application at all other voltages.

## Rule of Thumb -

Keep notch depth less than $10 \%$ if any other equipment will be connected to that same point of common coupling.

## Ithd and Vthd vs \%Load



What about Power Factor?

## What is Total Power Factor?

- Displacement PF
- COS of angle between fundamental current and voltage due to reactive current
- $P F_{\text {disp }}=\cos (\theta)=P / S_{1}$


$$
P F_{t o t a l}=P F_{d i s p} \times P F_{d i s t}=\frac{P[k w]}{S[k V A]}
$$

- Distortion PF
- Calculation based upon the current THD due to harmonic currents
- $P F_{\text {dist }}=\frac{1}{\sqrt{1+T H D^{2}}}=S_{1} / S$


## PF of a Motor Across the Line


\% Load

## PF of a Drive w/o LR or LC vs Load



## PF of a Drive w/LR or LC vs Load



## PF of an 18-Pulse Drive vs Load



## PF of an AFE Drive


\% Load

## End of Part 1



